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Some Challenges & Opportunities in the Field of Geotechnical & Soil-Structure-Interaction - (Geo-Structures)

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COLLEGE OF ENGINEERING

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Overview



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- Outstanding Questions in Soil Liquefaction
 - Laboratory vs. Field Behaviors
 - ~~System Response of Interlayered Soil Deposits~~
 - Partial Drainage and Multidirectional Loading
 - Liquefaction of Gravelly Soils
- Combined Loading on Deep Foundations (SSI Knowledge Gap)
 - Torsional response of deep foundations
 - Combined loading: torsional, lateral (axial?)

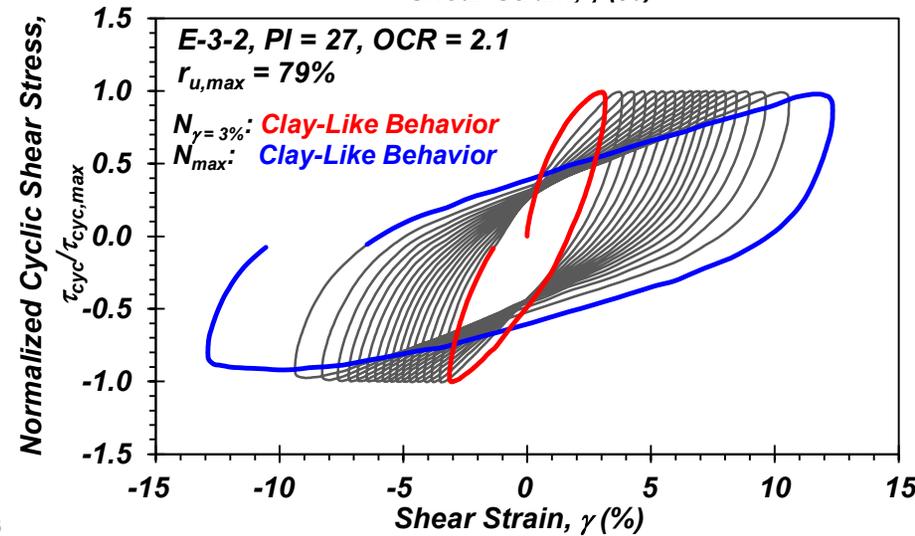
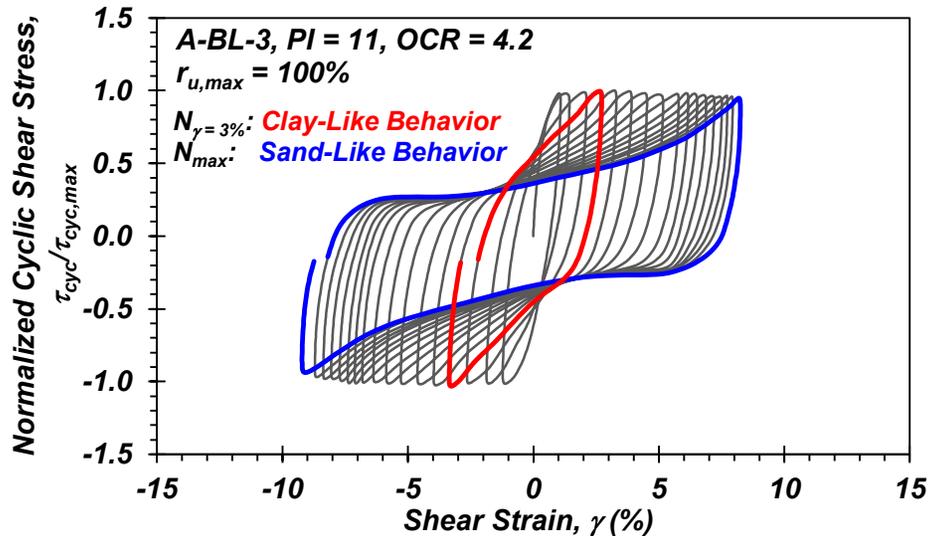
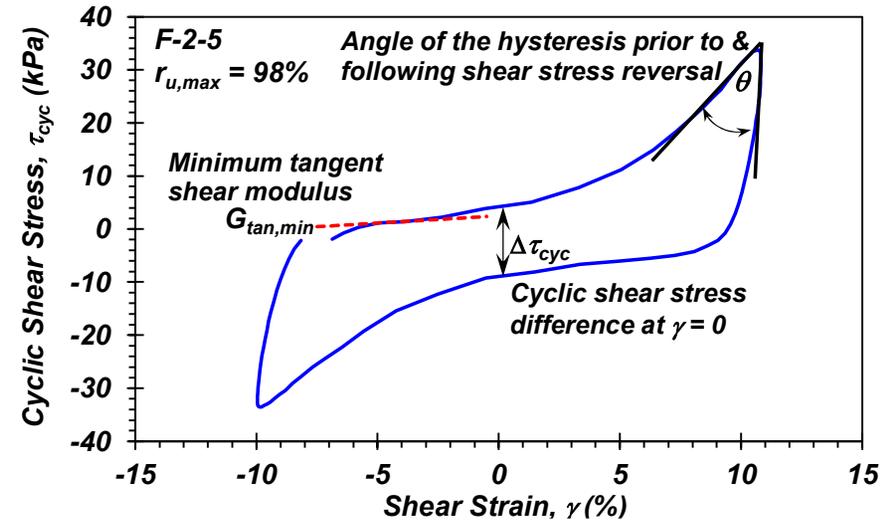
Outstanding Questions in Soil Liquefaction

Laboratory vs. Field Response

Linking Hysteretic Behavior to Liquefaction Susceptibility

Example behaviors @ $N_{\gamma=3\%}$ and N_{max}

Specimen	Behavior		$r_{u,max}$ (%)		$G_{tan,min}/\tau_{cyc,max}$		$\Delta\tau_{cyc}/\tau_{cyc,max}$	
	$N_{\gamma=3\%}$	N_{max}	$N_{\gamma=3\%}$	N_{max}	$N_{\gamma=3\%}$	N_{max}	$N_{\gamma=3\%}$	N_{max}
F-2-6	Interm.	Sand	93	99	10.12	0.00	0.60	0.47

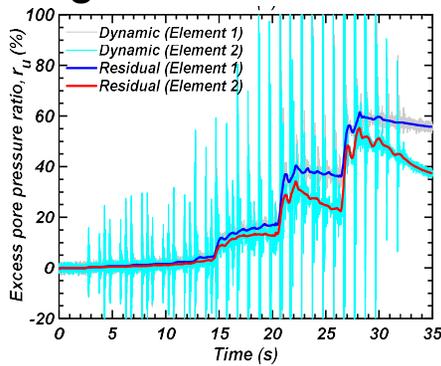


Laboratory vs. Field Response

Observed Field Behavior

Field Response?

- Specimens derived from the OSU Blast Array at Port of Longview, WA (Jana et al. 2023a)
 - Instrument array facilitates computation of stresses and strains with linkage to excess pore pressure generation
 - Loaded using “T-Rex” (NHERI@UTEXAS),
 $\gamma_{max} \approx 0.15\%$
 - Loaded using controlled blasting,
 $\gamma_{max} \approx 1.15\%$
- Goal: link laboratory and field responses



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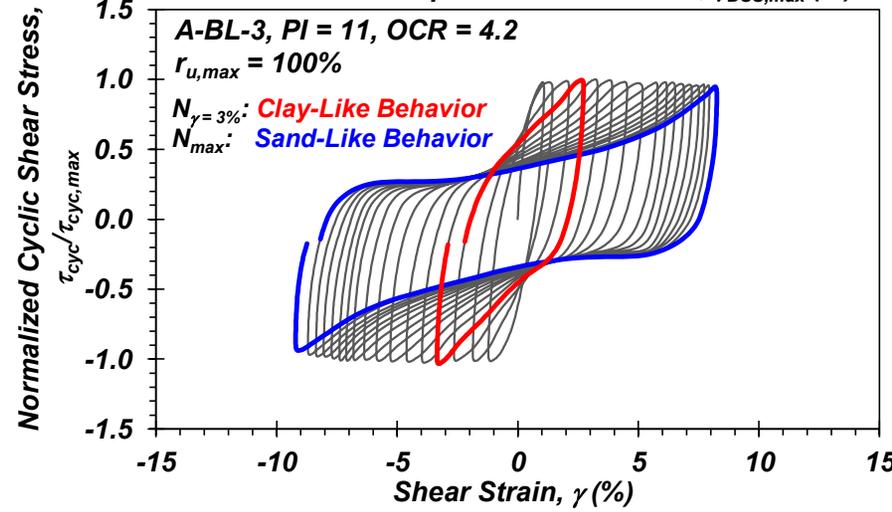
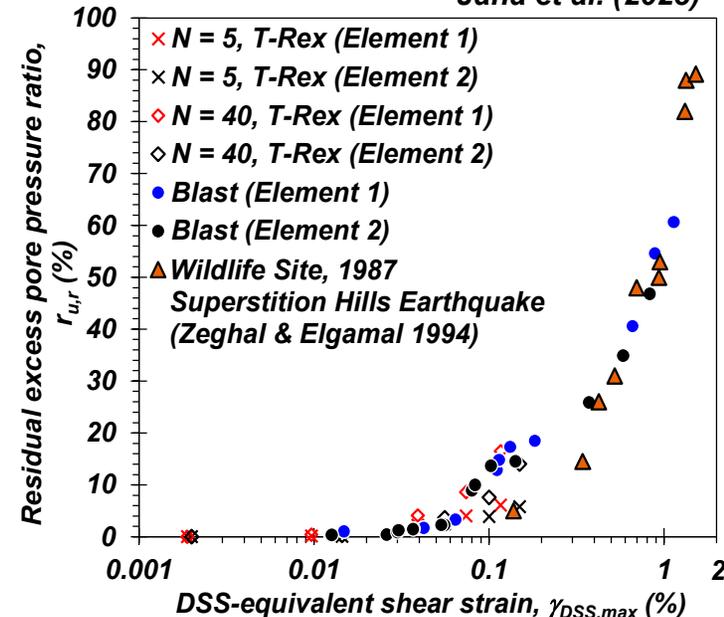


Laboratory vs. Field Response

Observed Field Behavior

- *In-situ* variation in residual excess pore pressure with shear strain; response similar to silty sand deposit @ Wildlife Site
- Large-strain “sand-like” cyclic behavior in CDSS linked to smaller strain liquefaction tendency
- Evidence suggests that:
 - Liquefaction of these transitional, low plasticity silts in the field is likely if loaded sufficiently
 - Ultimate hysteretic behavior ($\gamma > 5\%$) in CDSS is necessary to reveal the liquefaction potential (**susceptibility**)
 - Liquefaction in the field may occur at smaller strains than that implied by stress-controlled CDSS tests
- **LHPOST6 + laminar container may be used to prepare identical specimens (lab & container) to interrogate mis-match between laboratory and field**

Jana et al. (2023)



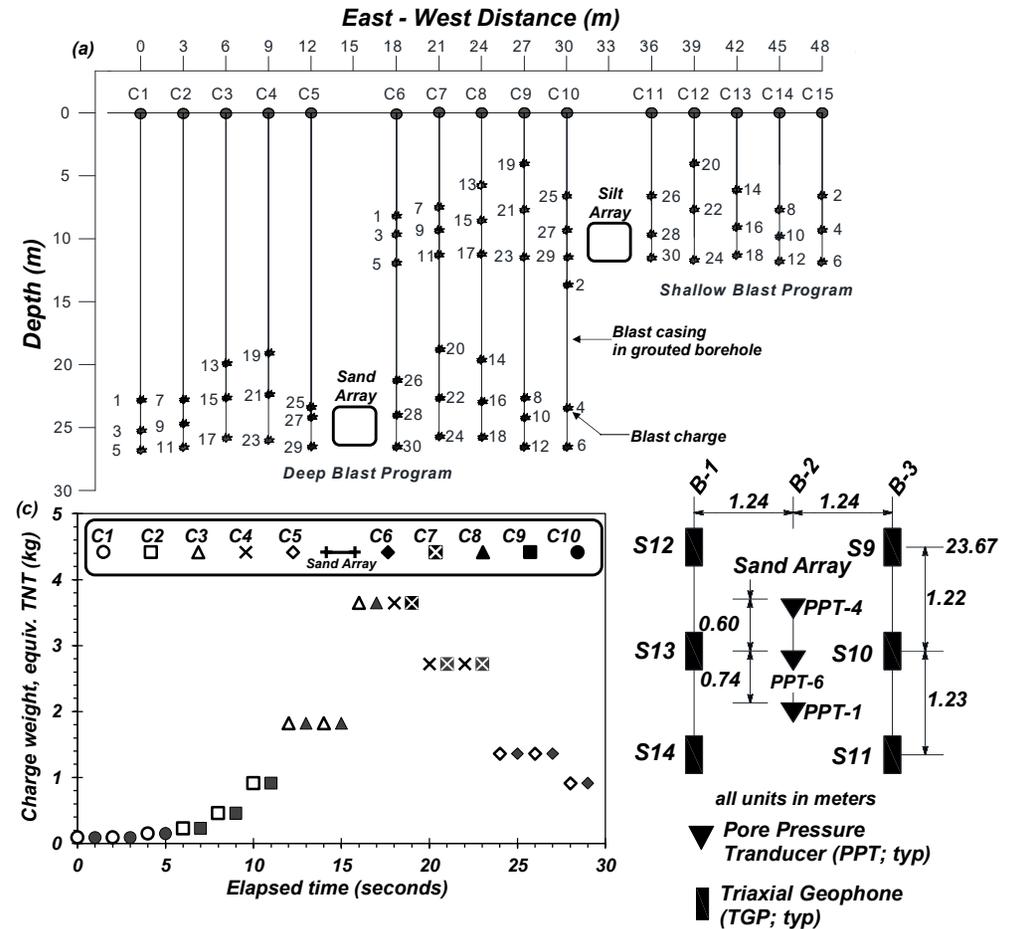
Partial Drainage & Multi-directional Shaking

Instrumentation Techniques



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- Full-scale, in-situ dynamic testing has demonstrated the viability of our instrumentation techniques
 - Velocity transducers placed to form “nodes” of a physical “finite” element
 - Piezometers placed at mid-points of elements to measure pore pressure
- Shear waves generated through detonation of explosives
- Shear strains through differentiation of displacement time histories
- Shear stresses through velocity time histories & V_s
- Shear modulus & damping



Field Experiments

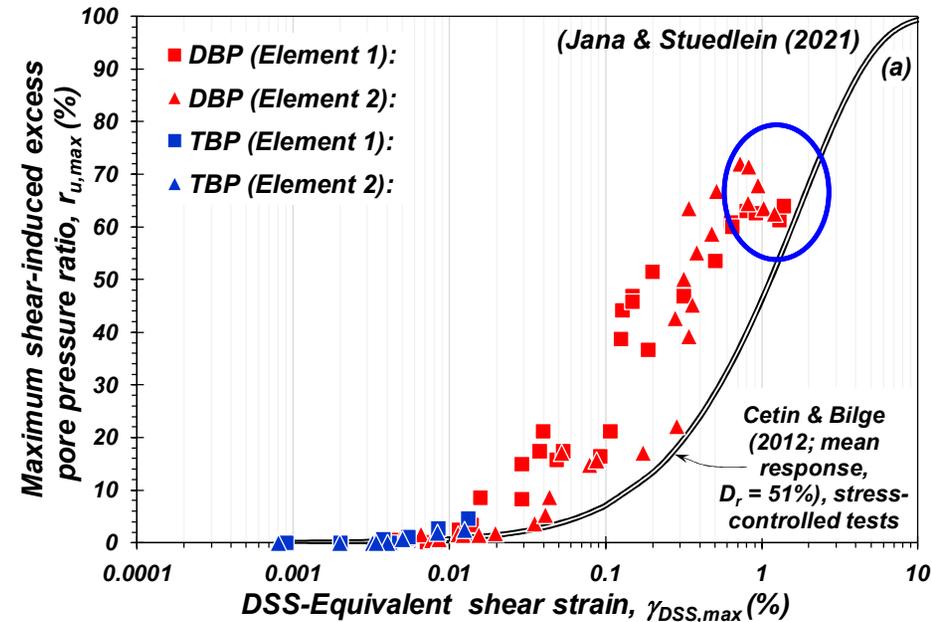
Controlled Blasting @ Depth of ~25 m



Key Observations (TBP & DBP)

Shear Strain vs. Excess Pore Pressure

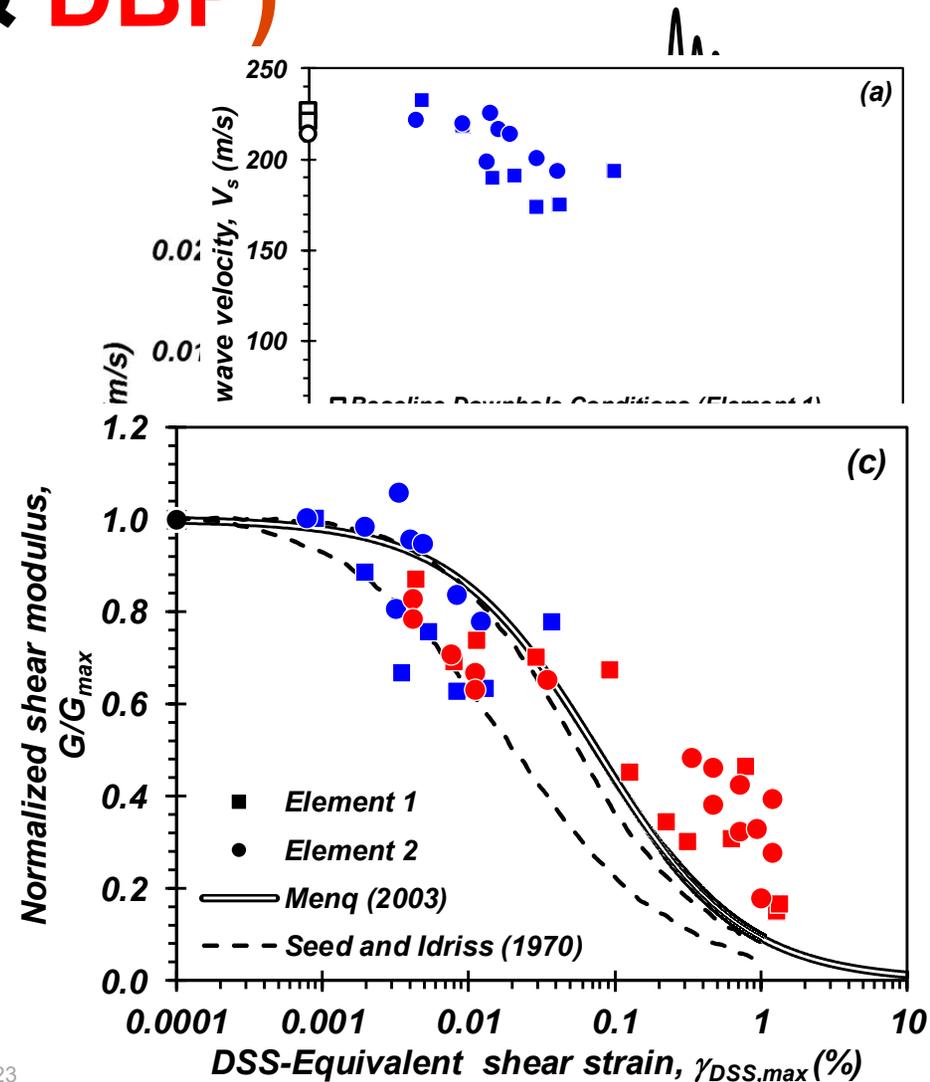
- Maximum excess pore pressure, $r_{u,max}$, occurs at smaller γ_{max} than implied by EPWP model for sands (C&B 2012)
- Drainage towards end of DBP inhibits larger $r_{u,max}$
- Strain-controlled CDSS data confirm γ - r_u relationship at v. small & large strains, until drainage initiates



Key Observations (TBP & DBP)

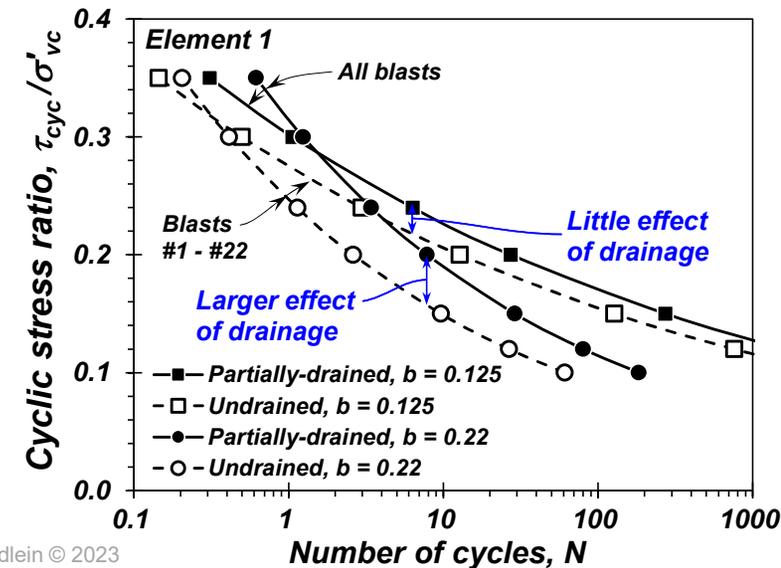
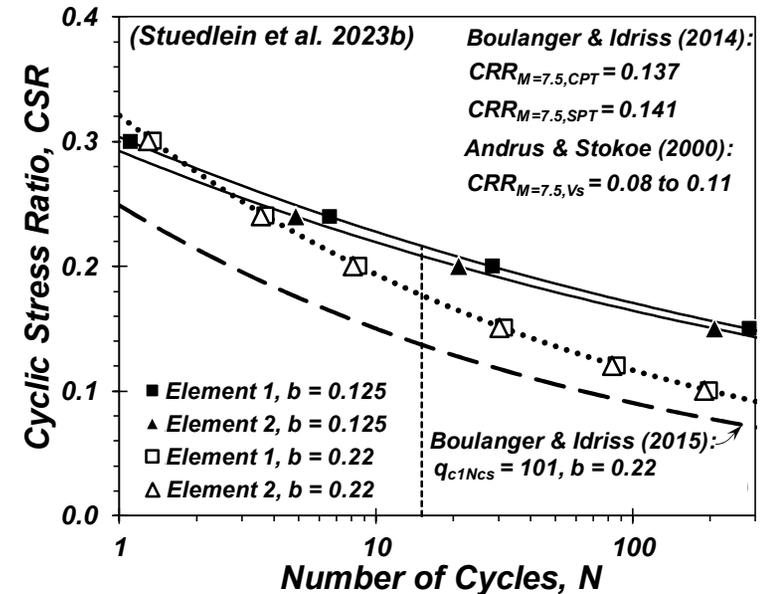
Shear Modulus Reduction with Shear Strain

- Baseline V_s established through downhole and cross-hole (blast) tests (TBP), and downhole (DBP)
- Shear wave velocity calculated for each charge as the waveform passes through the array
- V_s is matched with its corresponding shear strain
- Shear modulus deduced: $G_{max}, G = \rho \cdot V_s^2$
 - Initial loss of stiffness consistent with previously-reported laboratory data
 - Effects of multi-directional loading?
 - Large strain response indicative of field **drainage**



Outstanding Questions in Soil Liquefaction

- In-situ cyclic resistance > case history-based triggering estimates (*upper right figure*)
- Effects of drainage has been documented; partial drainage increases resistance (*lower right figure*)
- What are the effects of multidirectional shaking?
 - Blast-induced S-waves produce 2D or 3D shaking
 - Effect on cyclic resistance mixed – *needs further study*
- Blasting → 3D excess pore pressure field (?)
- Does partial drainage occur in the field?
 - Possible for long-duration (CSZ) earthquakes
 - *Need to confirm effects on shear modulus, amplification*
- **Propose construction of bidirectional laminar box to fully leverage LHPOST6 capabilities**



Liquefaction of Gravels

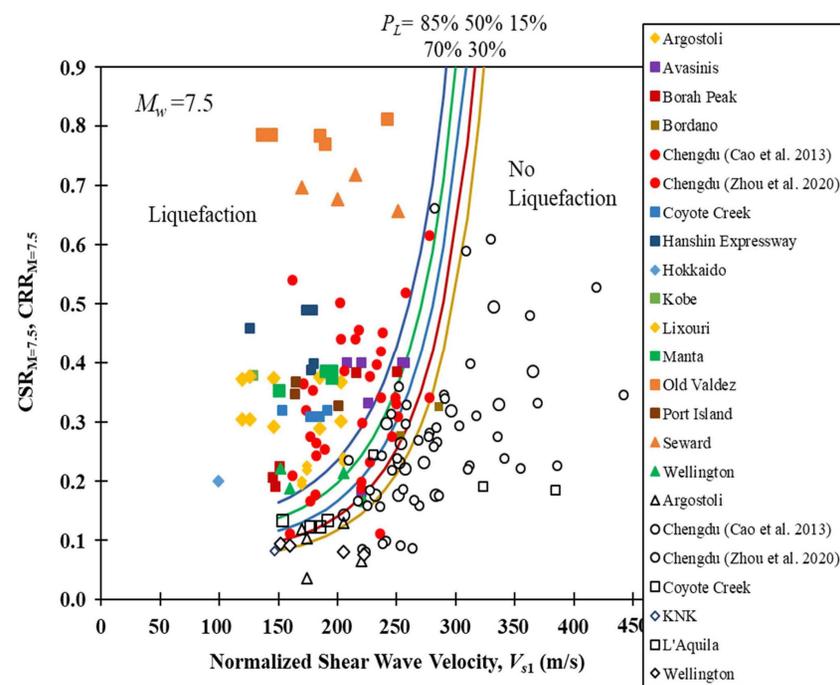
Liquefaction of Gravels

Concerns

- The coupled fluid-mechanical seismic response of natural, native gravelly soils *in-situ* has never been observed in a controlled experimental setting
- Penetrometer-based estimates of cyclic resistance
 - DPT – small penetrometer relative to some gravel sizes
 - BPT or iBPT: relies on correlations to SPT (?), not widely-available, \$\$\$
- Uncertainties with V_s -based methods
 - New case history-based V_s liquefaction model available – great..!
 - But what about those gravels that liquefied without surface manifestation? Epistemic uncertainty in model?



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Rollins et al. (2022)

Liquefaction of Gravels

Concerns, Variables, Hypothesis

- Epistemic uncertainty → reducible uncertainty
- Penetration resistance *can* account for effects of gradation through blow count, but subject to partial drainage when fine sand, silts, and clays comprise the matrix between large particles
- Gradation is key:
 - Poorly-graded gravels drain fast, but exhibit large void ratios and have lower V_s as a result; when capped, drainage is prohibited
 - Well-graded gravels cannot drain fast, but exhibit small void ratios, have larger V_s , and larger cyclic resistance as a result
- Demonstration via the cyclic strain approach

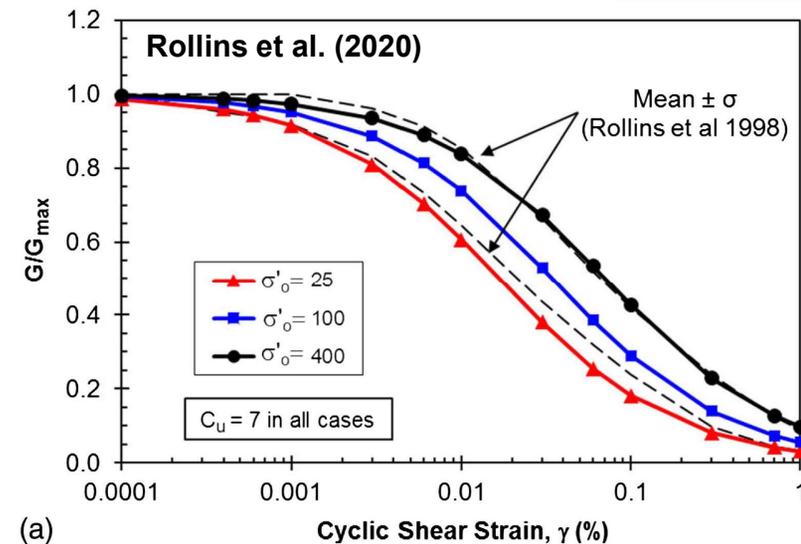
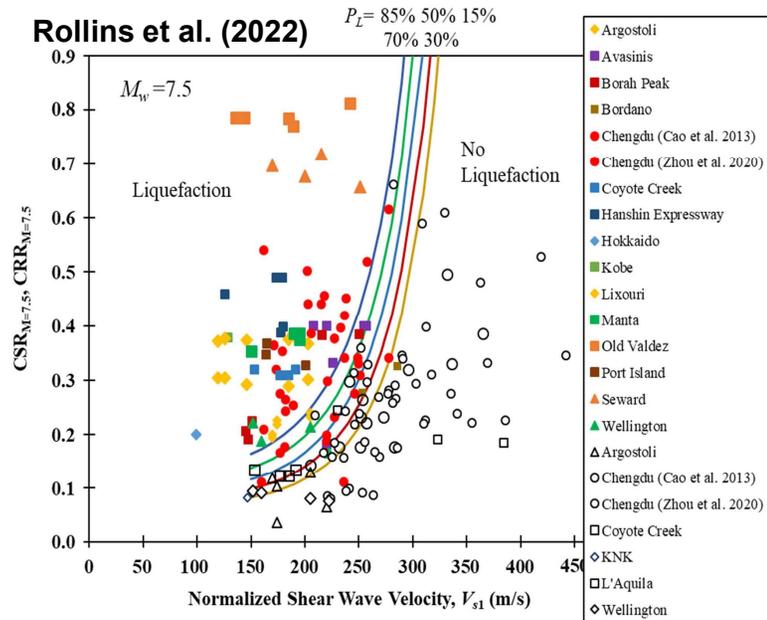
Liquefaction of Gravels

Cyclic Strain Approach

- Proposed in discussion to Rollins et al. (2022)
- Set CRR from V_s -based triggering model equal to that expected from shear modulus degradation \rightarrow probabilistic shear strain to trigger liquefaction, $\gamma_{cl}(P_L)$
- Allows coefficient of uniformity, C_u to be included in liquefaction triggering analyses

$$CRR = \exp\left(\frac{3.88 \cdot 10^{-7} \cdot V_{s1}^3 - 1.6 \cdot M_w - \ln\left(\frac{1-P_L}{P_L}\right)}{4.95}\right)$$

$$\frac{G_{cl}}{G_{max}} = \frac{1}{1 + \left(\frac{\gamma_{cl}}{\gamma_r}\right)^{0.84}}$$

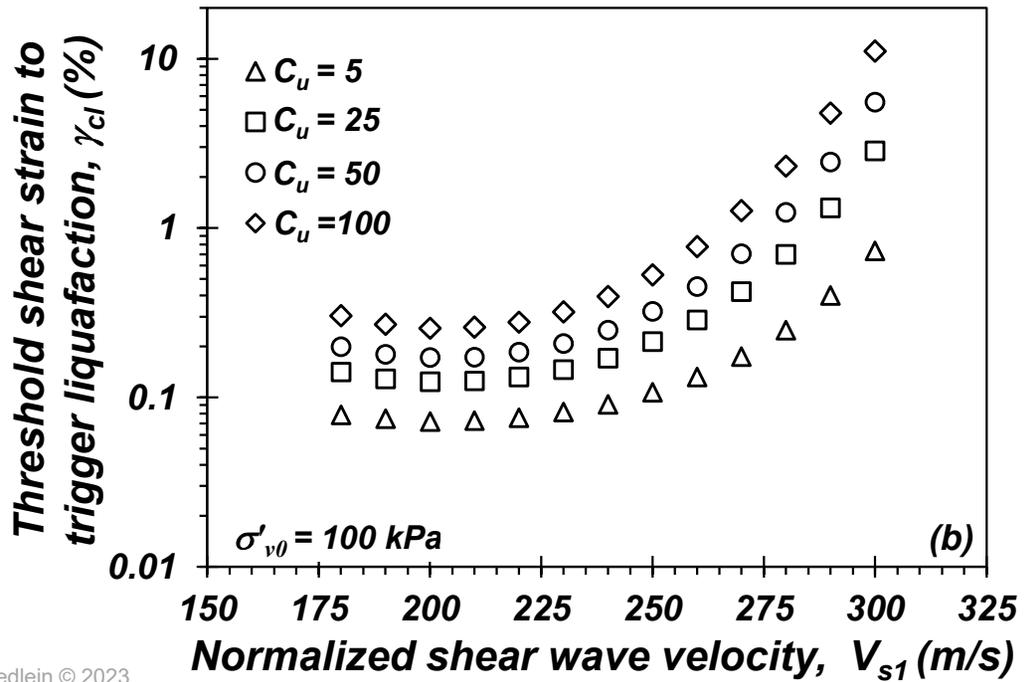
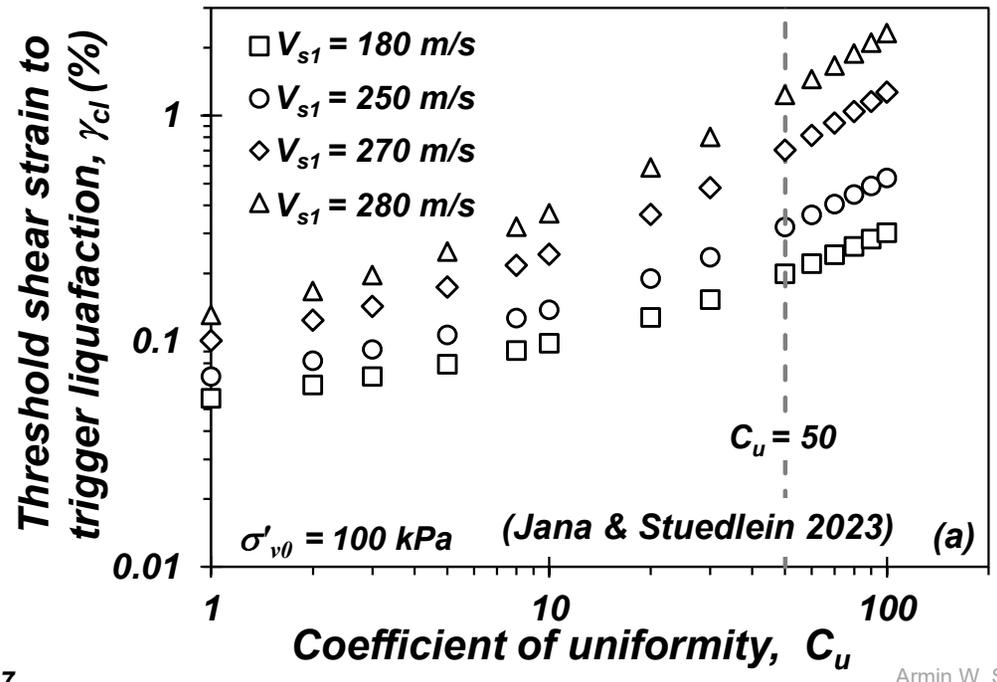


(a)

Liquefaction of Gravels

Proposed Cyclic Strain Approach (Jana & Stuedlein 2023)

$$\gamma_{cl} = \exp\left(\frac{3.88 * 10^{-7} V_{s1}^3 - 1.6 M_w - \ln\left(\frac{1 - P_L}{P_L}\right)}{4.95}\right) \left[\frac{\sqrt{\sigma'_{v0}}}{0.1 * \rho * V_{s1}^2} \right] \frac{1}{1 + \left\{ \frac{\gamma_{cl}}{0.0046 (C_u)^{-0.197} (\sigma'_{\nu})^{0.52}} \right\}^{0.84}}$$



Liquefaction of Gravels

Proposed Cyclic Strain Approach (Jana & Stuedlein 2023)

- Deterministic γ_{max} can be computed directly
- We determined C_u and γ_{max} for 70 of 174 case histories
- For all liquefaction (“Yes”) cases, except 3, $\gamma_{max} > \gamma_{cl}$
- For all “No” cases, except 5, $\gamma_{max} < \gamma_{cl}$ (effect of capping layer?)
- γ_{max} for 1964 Anchorage EQ very large for lateral spreading and flow slide case histories (sometimes exceeding 1,000%)
- ***We can measure γ_{max} in-situ or in a laminar container***
- *Thus, we can directly test our cyclic strain-based approach*

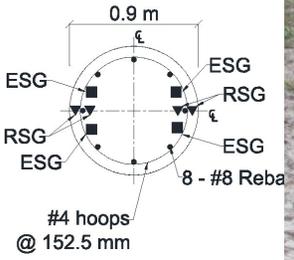
Combined Loading on Deep Foundations

Combined Loading on Deep Foundations

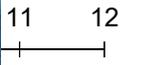
- Axial-lateral-torsional loadings
- Sources of combined loadings:
 - Mast arm signal- and signage poles (gravity, wind)
 - Near and offshore structures (berthing/mooring loadings)
 - Skewed bridges (seismic)
 - Asymmetric buildings (wind, seismic)
- These loadings can be extreme and are uncertain
- Resistance..? ODOT-funded study shed some light on this topic



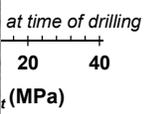
Instrumented, Full-scale Specimens



Northeast, A'
Distance (m)



- ▼ Min.
- ▽ ATD
- ▽ Test
- ▼ Max.



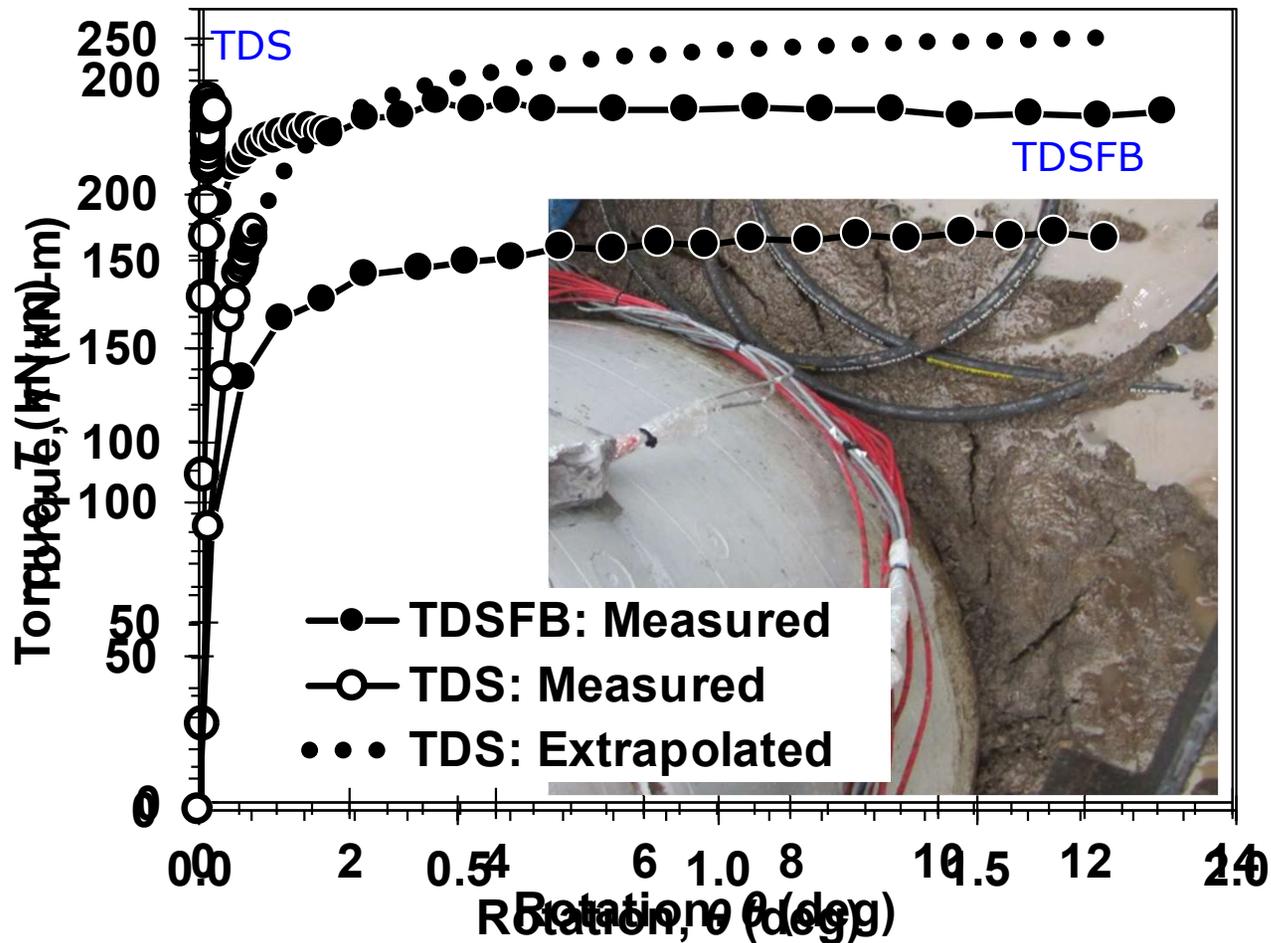
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Limits (%)

(MPa, 1 MPa = 145 psi)

Quasi-Static Torsional Loading

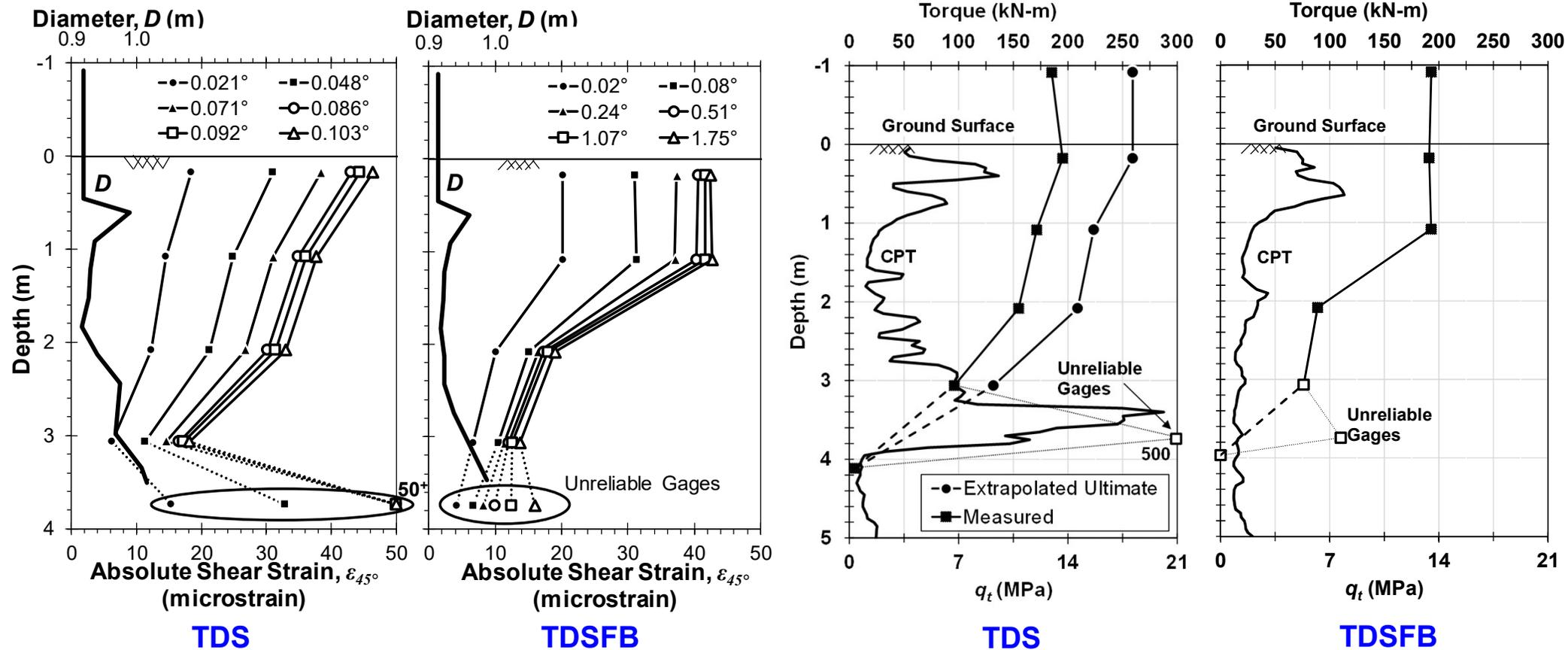
Applied Rotation at Head vs. Developed Torque



Take-away:
Torsional resistance is a “small” rotation (displacement) phenomenon

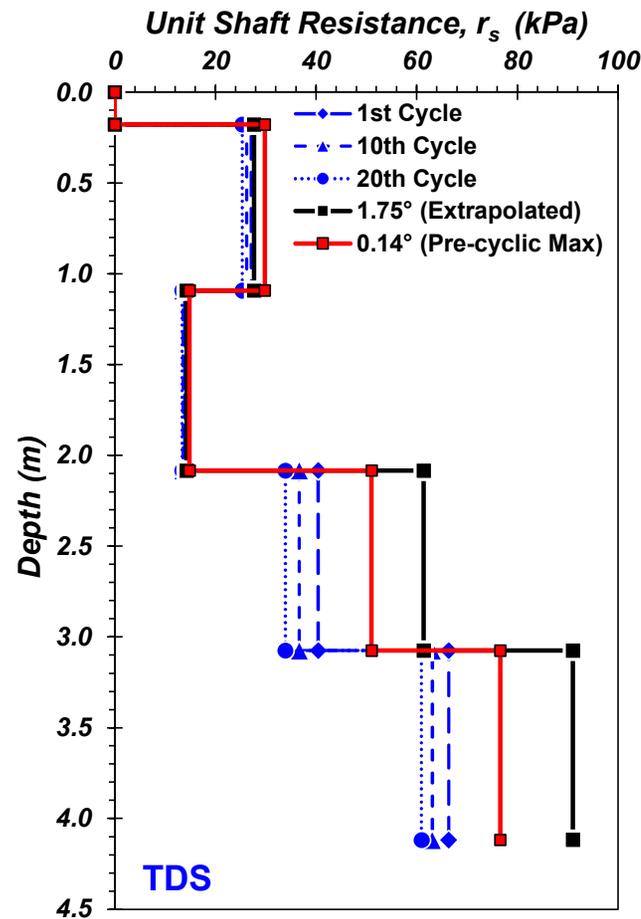
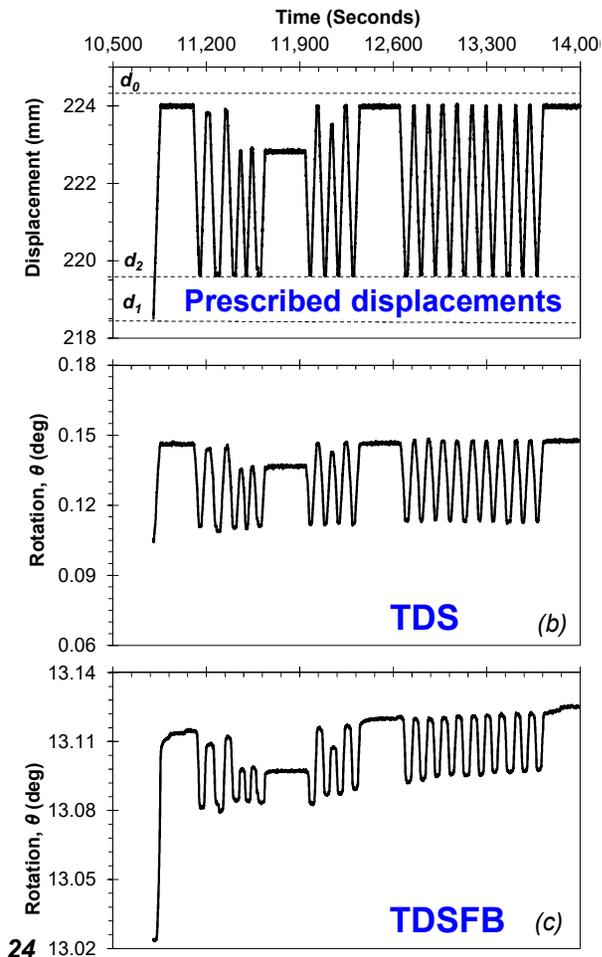
Quasi-Static Torsional Loading

Distribution of Shear Strain & Torsional Load Transfer



Quasi-Static Cyclic Torsional Loading

Loading Protocol, Global Response, Unit Shaft Resistances

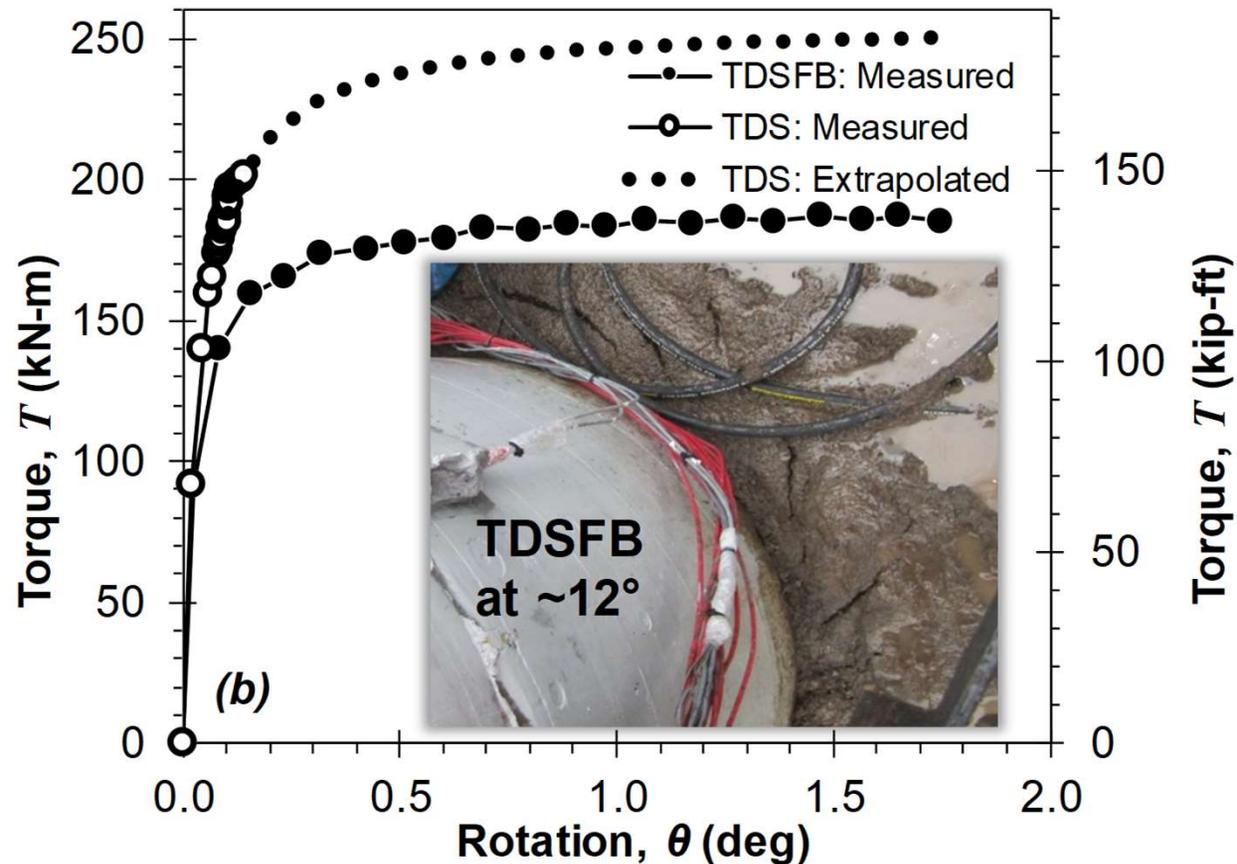


- No significant change in global torsional response with number of cycles
- Initial cyclic stiffness similar between both shafts, but post-yield stiffness for TDS 2x larger than for TDSFB due to dense sand layer
- Local response shows possible softening and/or friction fatigue

Combined Loading (*Incidental...*)

Recall:

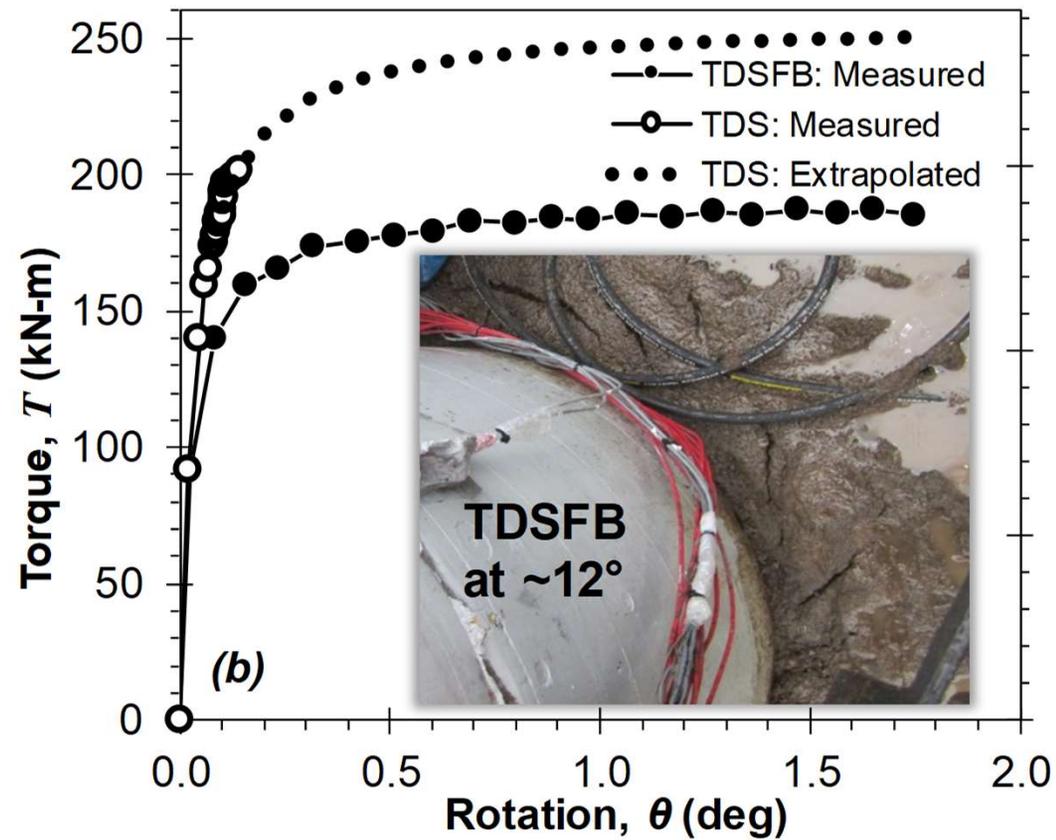
- Radial ground cracks opened next to TDSFB during torsional loading
- One shaft experienced “geotechnical failure”, the other did not...
- Differential mobilization of resistance under a displacement couple requires an induced lateral load for torsional equilibrium....
- Allows insight into effect of combined loading



Combined Loading

Significant Differences in Lateral Responses

- The initial response of TDS (no ground cracking) indicated little impact of combined loading
- Not so for TDSFB (with ground cracking)
- Torsional shear-induced cracks must first close prior to the generation of lateral resistance
- If torsional shear occurs prior to large lateral movements, then the lateral response will be soft.
- **Consider torsional loading prior to near-fault velocity pulse...**



Very little rotation required to mobilize ultimate torsional resistance...!

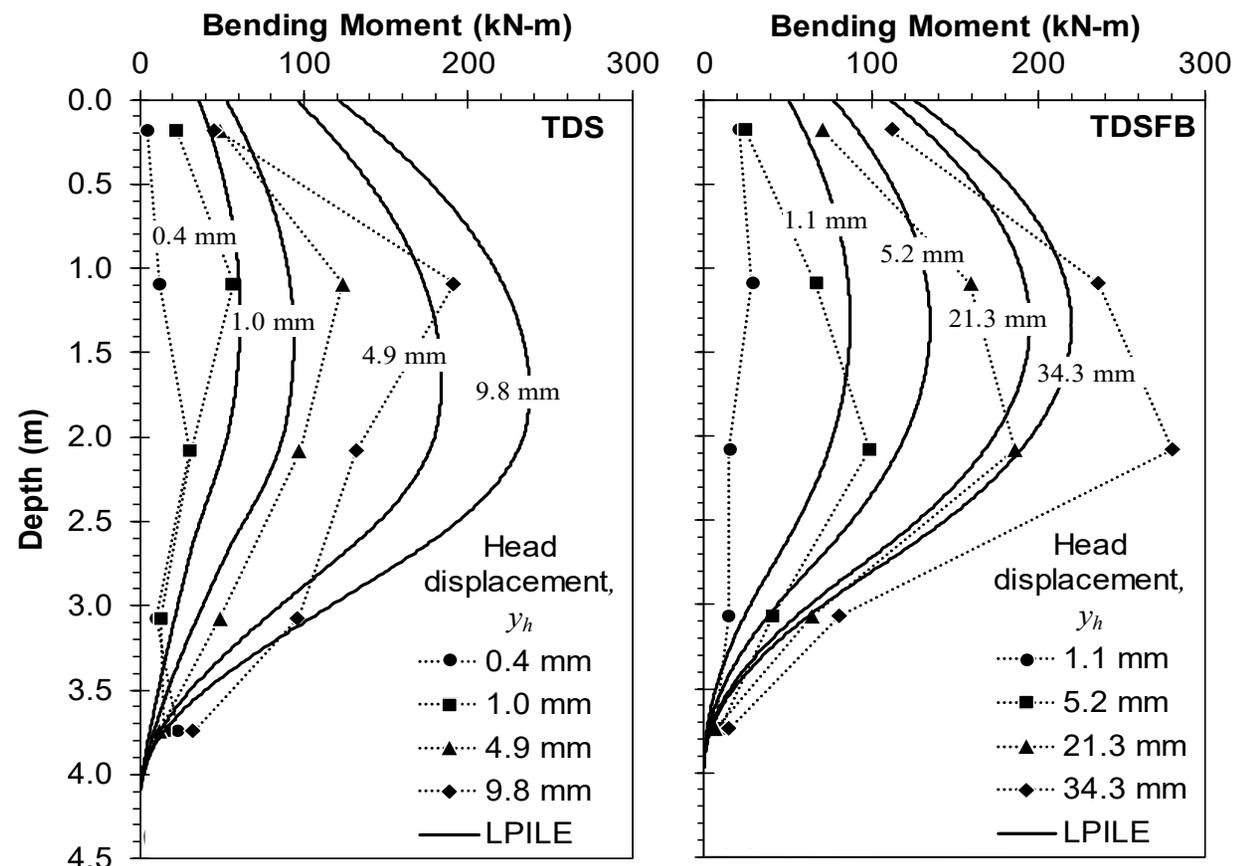
Combined Loading

Bending Moment Profiles; Poorly-captured using 1D Methods



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- Typical lateral loading simulation (e.g., L-Pile) cannot capture effect of combined flexure and torsional shear
- In case of TDSFB, the maximum bending moment was significantly under-predicted as a result
- **LHPOST6 + Laminar Box: apply controlled torsional, and inertial and kinematic lateral loading to study effects of combined loading, develop numerical methods for simulation**



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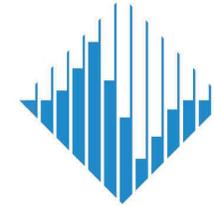
Acknowledgements

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Work Cited



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